

ISOTHERMAL MODELLING BASED EXPERIMENTAL STUDY OF DISSOLVED HYDROGEN SULFIDE ADSORPTION FROM WASTE WATER USING EGGSHELL BASED ACTIVATED CARBON

(Model Isoterma Berdasarkan Kajian Penjerapan Hidrogen Sulfida Terlarut daripada Air Sisa Menggunakan Karbon yang Diaktifkan Berasaskan Kulit Telur)

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Abstract

This paper reports on the experimental work using batch process conducted to determine the adsorption capacity of dissolved hydrogen sulfide in the synthetic wastewater onto the activated carbon which is derived from the eggshell. Fourier Transform Infrared Spectroscopy (FTIR), Energy-Dispersive X-ray Spectroscopy (EDX), Scanning Electron Microscopy (SEM), and particle size distribution have been used to characterize the prepared material. The raw materials of chicken eggshell are adopted to retrieve the carbon content which is then activated using KOH as the activation agent. The examined concentration of dissolved hydrogen sulfide is ranging from 100 to 500 ppm. The maximum adsorption capacity of the dissolved H₂S onto the activated carbon is 289.3 mg/g and the equilibrium time is 6 hours. The examined pH value in this study is ranging from 4.5 to 5.5. The two well-known equilibrium adsorption isotherm models, i.e. the Langmuir and the Freundlich models, are employed. It is found that the adsorption isotherm capacity agrees very well to the Freundlich isotherm model. This paper attempts to show the difficulties of converting CaCO₃ to carbon due to the fact that the raw material contains higher calcium (Ca) content instead of carbon. It is concluded that the carbon derived from the chickens' eggshells is very beneficial for treatment of dissolved H₂S in waste water.

Keywords: adsorption, hydrogen sulfide, chicken eggshells, activated carbon, isotherm

Abstrak

Kajian ini melaporkan mengenai kerja eksperimen menggunakan proses kelompok yang dijalankan untuk menentukan kapasiti penjerapan hidrogen sulfida terlarut dalam air sisa sintetik ke dalam karbon yang diaktifkan dihasilkan daripada kulit telur. Spektroskopi Inframerah Fourier (FTIR), Spektroskopi X-ray Tenaga Serakan (EDX), Mikroskop Imbasan Elektron (SEM), dan taburan saiz zarah telah digunakan untuk mencirikan bahan yang disediakan. Kulit telur ayam sebagai bahan mentah telah digunakan untuk mendapatkan semula kandungan karbon yang kemudiannya diaktifkan dengan menggunakan KOH sebagai agen pengaktifan. Julat kepekatan hidrogen sulfida yang diperiksa adalah di antara 100 hingga 500 ppm. Kapasiti penjerapan maksimum H₂S terlarut ke dalam karbon diaktifkan adalah 281 mg/g dan masa keseimbangan selama 6 jam. Julat nilai pH yang diperiksa dalam kajian ini di antara 4.5 hingga 5.5. Kedua-dua model penjerapan isoterma keseimbangan terkenal seperti model Freundlich dan Langmuir telah dilaksanakan. Kapasiti penjerapan isoterma didapati selari dengan model isoterma Langmuir. Kajian ini cuba menunjukkan kesukaran untuk menukar CaCO₃ kepada karbon disebabkan oleh bahan mentah mengandungi

kandungan kalsium (Ca) yang tinggi dan bukannya karbon. Ini dapat disimpulkan bahawa karbon yang diperolehi daripada kulit telur ayam adalah sangat bermanfaat untuk rawatan H₂S terlarut dalam air sisa.

Kata Kunci: penjerapan, hidrogen sulfida, kulit telur ayam, karbon diaktifkan, isoterma

Introduction

Hydrogen sulfide (H₂S) is a very toxic, corrosive and flammable gas. It is a colorless gas, best known for its strong smell, much like the strong nauseating smell of rotten eggs. The H₂S is volatile in water and soluble in some polar organic solvents [1]. It is also a reducing agent and oxidizes easily when the conditions are right and corrodes metals and even concrete. For example, H₂S will oxidize gradually to elemental sulfur and over time oxidize to sulfuric acid and eventually damage the sewer [2]. Under specific conditions such as at a low concentration (1.36 mg/L) pH between 3 to 5 and immersion time of more than two hours, H₂S has been found to have an inhibiting effect on iron corrosion [3, 4]. Moreover, H₂S is also a harmful and putrid gaseous compound. It can create health problems, like coma, irritated eyes, and respiratory system irritation. Furthermore, the human nose can detect H₂S at concentrations as low as 0.5 part-per-billion-volume (ppbv) [5]. Therefore, excess exposure to H₂S can cause both chronic and acute ramifications [6]. Surprisingly, the allowable limit of H₂S in drinking water is not specified by the World Health Organization (WHO) [7]. Most of the sulfide found in water may be expected to exist as molecular H₂S at pH less than 4 [8]. Bisulfide and sulfide ions can be found when H₂S is dissolved in water as per the following reaction:



Reaction 2 (reverse direction) occurs at pH < 4.5 [9] and reaction 3 (forward direction) happens at pH ≥ 9 [10]. In a natural environment, acid rain is precipitated through the oxidation of H₂S to sulfuric acid. H₂S dissolves easily in water (4-6 g/L) and it is poisonous to almost all types of life forms [11]. Owing to the above reasons, various agencies have been consistently developing solutions to remove H₂S. It could be removed in three different ways such as adsorption, oxidation, and scrubbing. Recently, there is a renewed interest in using adsorption process as an effective method to remove the pollutant e.g. H₂S from wastewater. Adsorption is a physio-chemical technique, involving mass transfer between the liquid and the solid phase [12]. A considerable amount of literatures detailing on the removal of H₂S have been published [13-15]. These studies have reported that the adsorption rate of H₂S is affected by many factors such as surface area of adsorbent, pore size, moisture content, pH, and surface chemistry (oxygen containing functionalities). The experimental and simulation study detailing on H₂S adsorption on impregnated activated carbon under an anaerobic condition has been carried out by Xiao et al. [13]. They have applied a sodium carbonate impregnated activated carbon as the adsorbent for low concentration H₂S in nitrogen under the anaerobic condition in a fixed bed [13]. Moreover, sludge-derived H₂S adsorbents have received considerable attentions from the galvanizing industry [14].

Other study has been conducted by Guo et al. [15], whereby they have studied activated carbons derived from oil-palm shell as an adsorption of H₂S [15]. In addition, study on ferric and alum water treatment residuals has been conducted by Wang and Pei [16]. Possible materials to be used as adsorbents of H₂S such as Fine Rubber Particle Media (FRPM) and crushed oyster shell have been tested by Wang [17] and Asaoka [18], respectively. Recently, the low-cost carbon-based materials such as agricultural wastes have been used as pollutant adsorbent such as rice husks [19], banana and orange peels [20], coconut shell [21], macadamia nut shells [22], fibers of oil palm empty fruit bunches [23], rice straw [24]. Several studies have documented that activated carbon has been widely used as an adsorbent for achieving high water purification. So far, very little attention has been paid to remove H₂S from wastewater in liquid phase.

Therefore, this paper addresses on the use of eggshells as the source of activated carbon to adsorb dissolved H₂S as liquid form out of wastewaters. It is important to note that eggshells are abundant and environmental friendly [25]. In this paper, our objective is to assess the effectiveness of activated carbon derived from eggshell waste as an adsorbent of dissolved H₂S from waste water. Also, we aim to characterize this adsorbent and find the suitable isotherm adsorption model to be fitted with this adsorption process.

Materials and Methods

Preparation of activated carbon

In this study, the activated carbon derived from eggshells has been used as an adsorbent of H₂S appeared in the petroleum refinery synthetic waste water. Firstly, the eggshells (around 100 pieces) were collected from restaurants around Kajang, Selangor, Malaysia. A sample of the eggshells was then carefully rinsed several times with deionized water and acidic solvent to remove impurities and pollutants. After that, the sample was gradually dried under 105 °C for eight hours. Then the dried eggshell was grinded into powder form. The powder (10 g) was placed in a furnace and gradually heated up to 700 °C [26], at constant heating rate of 10 °C/min with nitrogen (N₂) flow rate of 150 mL/min. Then the result product was soaked in concentrated solution of KOH for 24 hours. After that, it is filtered and dried under 105 °C. Finally, the activation process is done in a horizontal tubular furnace at temperature of 750 °C, which is subjected to constant heating rate of 10 °C/min with N₂ flow rate of 150 mL/min. The prepared material was coded as ACES.

Characterization of activated carbon

In this study, the pH value of the carbon surface was measured by taking a sample of 0.4 g of dry carbon powder added to 20 mL of water and the suspension was stirred overnight to reach equilibrium. Then, the pH value of the suspension was measured. Moreover, the surface morphology of the sample was examined using a Scanning Electron Microscope (SEM). Elemental analysis on the chemical composition of the sample was conducted using the energy-dispersive X-ray spectroscopy (EDX). The particle size distribution was also measured. The Fourier Transform Infrared Spectroscopy (FTIR) analysis has been used for the examination of functional groups on the surface of adsorbent.

Hydrogen sulfide solution

In this study, the synthetic waste water was prepared according to the procedure reported by Asaoka et al. [18]. A portion of Na₂S.9H₂O was dissolved in 500 mL solution of 0.01 M KCl purged with N₂ gas. Thereafter, the pH of the solution was adjusted to 4.5 – 5.5 using 0.2 M HCl [18]. The concentration of dissolved H₂S in water is 4 – 6 g/L [11]. All forms of H₂S are harmful to organisms, and they can exist in a solution in three forms, i.e. hydrogen sulfide (H₂S), bisulfide (HS⁻) and sulfide (S²⁻) [27].

Batch equilibrium studies

The adsorption capacity of the ACES has been carefully studied by examining its ability in removing H₂S from synthetic wastewater. The pollutant concentration was initially measured. The pH of the solution was controlled to 4.5 – 5.5 using NaOH and HCl. The experiments of the adsorption process of H₂S were conducted using a batch mode process. For each experiment, the adsorption was carried out using 0.1 g of adsorbent after degassing at 105 °C for 24 hours in the oven. The solution was rotated at 160 rpm with an electric shaker for 9 hours to test their adsorption capacities. Upon the filtration of the suspensions, the initial and final concentration were measured. The adsorption capacity of the pollutants was calculated using equation 4 below:

$$q_e = \frac{(C_0 - C_e)V}{m} \quad (4)$$

where V is the solution volume (L), m is the adsorbent amount (g), C_0 and C_e are the initial and final concentrations of the pollutants, and (q_e) is adsorption capacity in mg/g. All adsorption experiments were repeated and the maximum deviation was within 5%. All the measurements were done at fume hood as H₂S is a very dangerous gas. The adsorbent sample yield can be calculated using the following equation 5 below:

$$\text{Yield}(\%) = \frac{W_c}{W_o} \times 100\% \quad (5)$$

where W_c and W_o are the dry weight of the final sample (g) and the dry weight of precursor (g), respectively. The equilibrium data were then fitted using the adsorption isotherm models, namely the Langmuir and the Freundlich models.

Adsorption isotherm models

The adsorption isotherm models explained the connection between the amounts of adsorbate adsorbed per unit mass of adsorbent (equilibrium adsorption capacity, q_e) at constant temperature and adsorbate's concentration at equilibrium conditions (C_e). Langmuir and Freundlich models are considered the well-known equilibrium adsorption isotherm models, and they were employed in the current study. Langmuir isotherm assumes monolayer adsorption onto a surface containing a finite number of adsorption sites of uniform strategies of adsorption with no transmigration of adsorbate in the plane of surface [28]. The linear form of Langmuir's isotherm model is given by the following equation 6 below:

$$\frac{C_e}{q_e} = \frac{1}{Q_{max} K_L} + \left(\frac{1}{Q_{max}}\right) C_e \quad (6)$$

where C_e is the equilibrium concentration of the adsorbate (H_2S) (mg/L), q_e is the amount of adsorbate adsorbed per unit mass of adsorbent (mg/g), and parameters such as Q_{max} and b are Langmuir constants related to monolayer adsorption capacity and affinity of adsorbent towards adsorbate, respectively. The essential characteristics of the Langmuir isotherm can be expressed in terms of a dimensionless equilibrium parameter (R_L), which is defined by:

$$R_L = \frac{1}{1 + bC_0} \quad (7)$$

where C_0 is the H_2S initial concentration (in mg/L). The value of R_L indicates the type of the isotherm to be either unfavorable, linear, favorable, or irreversible as reported in Table 1.

Table 1. The range values of R_L

Value of R_L	Type of isotherm
$R_L > 1$	Unfavorable
$R_L = 1$	Linear
$0 < R_L < 1$	Favorable
$R_L = 0$	Irreversible

The Freundlich isotherm is another adsorption isotherm model which assumes heterogeneous surface energies, in which the energy term in Langmuir equation varies as a function of the surface coverage [29]. The correlation coefficients (R^2) is used to judge the applicability of an isotherm model. The well-known logarithmic form of the Freundlich model is given by the following equation 8 below:

$$\log q_e = \log K_F + \frac{1}{n} \log C_e \quad (8)$$

where q_e is the adsorption capacity at equilibrium (mg/g), C_e is the equilibrium concentration of the adsorbate (H_2S) and K_F and n are Freundlich constants.

Adsorption kinetic models

Normally, the pseudo-first-order, pseudo-second-order and other kinetic models are used to simulate adsorption kinetics and determine the reaction rates. The mathematical relations of pseudo-first-order and pseudo-second-order are as given in equations 9 and 10, respectively [30,31]:

$$\log(q_e - q_t) = \log q_e - \frac{k_1}{2.303} t \quad (9)$$

$$\frac{1}{q_t} = \frac{1}{k_2 q_e^2} + \frac{1}{q_e} t \quad (10)$$

where q_e and q_t are the H_2S adsorbed (mg/g) at equilibrium and at time t (h), respectively. k_1 (h^{-1}) and k_2 (g/mg h) are the rate constants for pseudo-first-order and pseudo-second-order, respectively.

Results and Discussion

Textural characterization of prepared activated carbon

Table 2 shows the composition of eggshell after the carbonization process. As seen, the prepared materials showed a high of carbon and oxygen of 30.36% and 50.27%, respectively. Indicating the carbon structure of the prepared material. Calcium is lower as compared to carbon and oxygen, which is could be attributed to remaining component of eggshells. Furthermore, the morphology of the adsorbent surface was tested using SEM, it is interesting to find that the extural structure of the ACES particles has porous structure with fine pores and cracks as shown in Figure 1. The porous materials is preferable for the adsorption processes as it will discussed in the coming sections.

Table 2. The elemental composition of ACES

Element	Weight %	Weight Error ($\pm$)
Carbon (C)	30.36	0.47
Oxygen (O)	50.27	0.86
Molybdenum (Mo)	6.16	0.31
Calcium (Ca)	12.48	0.31
Potassium (K)	0.40	0.07
Magnesium (Mg)	0.33	0.07
Total	100.00	

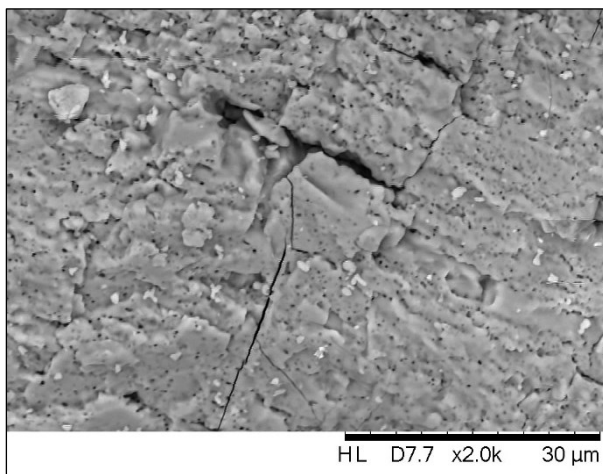


Figure 1. SEM image of ACES

Figure 2 shows the particle size distribution of adsorbent and Figure 3 shows another analytical test which is reporting on the FTIR structure of ACES particle. From Figure 3, it is obvious that the FTIR spectrum of ACES reveals three peaks. Each peak represents different functional group which might play an important role in the adsorption process. This corresponds to the presence of OH (hydroxyl), C=C (alkynes), and C=O (anhydrides) derivatives. Therefore, these surface functional groups could enhance the adsorption capacity of acidic pollutant (dissolved H_2S) in the waste water. Apart from that, at lower pH, the H^+ component which is high in concentration

may increase the positively charged CaOH^{2+} . It has been indicated that some reactions might occur during the adsorption process on the surface of adsorbent. Hence, reaction outlined in equation (11) might happen due to the oxygen content supporting the carbonization process of raw material. However, the dissociation of calcium oxide in water outlined in equation (12) forms calcium hydroxide (Ca(OH)_2) on the surface of ACES adsorbent which might help the adsorbent to attract via active site the acidic pollutant such as H_2S . Moreover, in equation (13) the OH^- from Ca(OH)_2 reacts with H_2S to form Ca(HS)_2 which is then converted to element sulfur as demonstrated in equation (14).

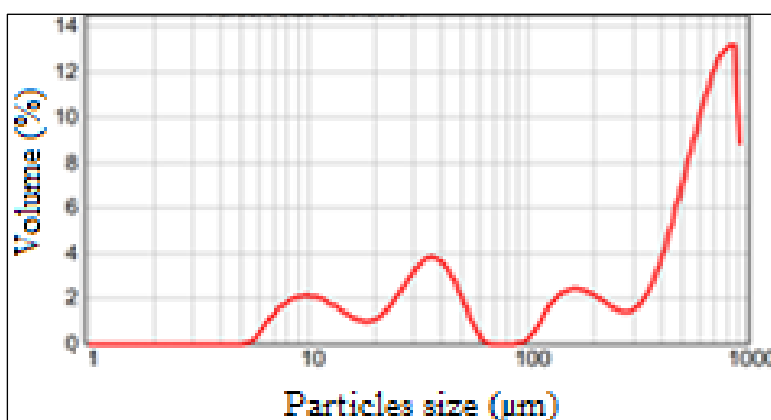


Figure 2. The particle size activated carbon derived from eggshell

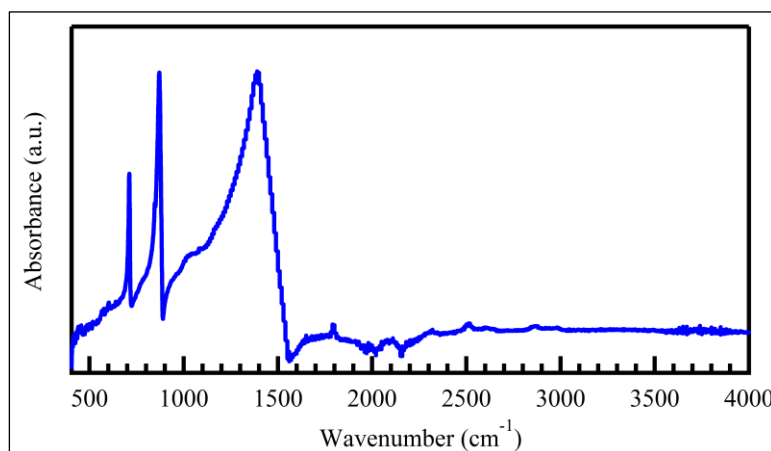


Figure 3. FTIR spectra of the ACES

Effect of contact time and initial hydrogen sulfide concentration on adsorption equilibrium

A series of contact time experiments for H₂S have been carried out at different initial concentrations (100 – 500 mg/L) and at temperature of 30 °C. Figure 4 shows that the equilibrium time of 6 hours is required for H₂S removal with the higher range of initial concentration (300 – 500 mg/L). However, with lower initial concentrations range (100 – 200 mg/L), a equilibrium time of 5 hours is required. As can be clearly seen from Figure 4, the amount of adsorbed H₂S onto the modified adsorbent (ACES) increases with time and it reaches an asymptote as time progresses. The results reveals that the H₂S adsorption rate is high at the initial stage of the contact period, and it becomes slower thereafter. This phenomenon happens due to the activity of functional group on the surface of adsorbent. It has been noted that vacant surface sites are vastly available for adsorption during the initial stage. However, as time elapses, it is difficult to occupy the remaining vacant surface sites due to the repulsive forces between the solute molecules on the solid and bulk phases. The results of this study indicate that the initial concentration has an important role in the adsorption capacity. Similarly, Choo et al. has found that higher concentration yields enhanced driving force along the pores, resulting in higher adsorption capacity [32]. However, Xiao et al. have shown that the effect of concentration is lower [13]. The contact time affects the adsorption capacity as well. From the current study, the effects of driving force and mass transfer are minimal in the dynamic adsorption. Moreover, it is limited by the rate of molecular diffusion into deeper pores and the adsorption process. The percentage of removal of H₂S is 43%, which is calculated using equation 15 below:

$$\text{Removal (\%)} = \frac{C_0 - C_e}{C_0} \times 100 \quad (15)$$

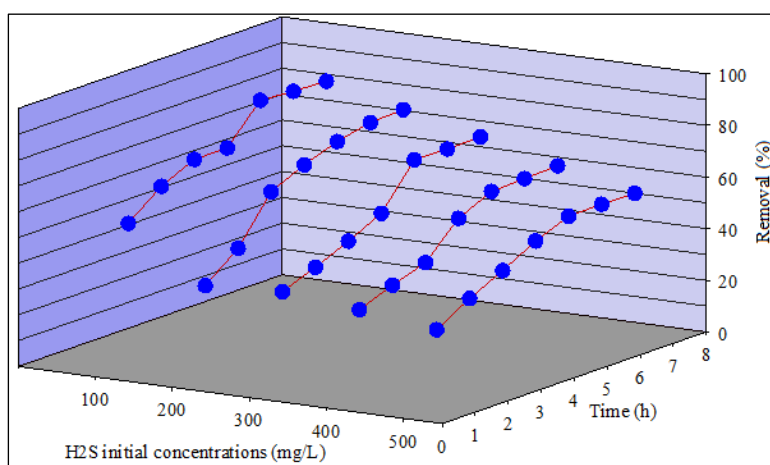


Figure 4. Effect of agitation time on H₂S adsorption onto ACES at various initial concentrations (100 – 500 mg/L)

Adsorption isotherms

The adsorption isotherm demonstrates the adsorption process when it reaches an equilibrium state. It reveals on how the adsorption molecules are distributed between the solid phase and the liquid phase. The analysis of the isotherm data, which is performed by fitting the data on different isotherm models, is an important step to find the suitable model that can be used for design purposes [33]. Basically, adsorption isotherm is important to describe how solutes interact with adsorbents, and is critical in optimizing the use of adsorbents. R^2 value is used to identify the appropriate model of the adsorption process. Figure 5 shows the Langmuir isotherm model, where $1/q_e$ changes linearly with $1/C_e$, at a slope of $1/Q_0b$. The Langmuir constants b and Q_0 are shown in Table 3. R^2 is 0.97, indicating that the fitting error is quite high compare with Freundlich isotherm model. To support that, the essential characteristics of the Langmuir isotherm can be expressed in terms of a dimensionless equilibrium parameter (R_L),

and the value of R_L is 0.069. Indeed, this indicates that the Langmuir isotherm is favorable for the adsorption of H_2S by the ACES under the working conditions considered in this study.

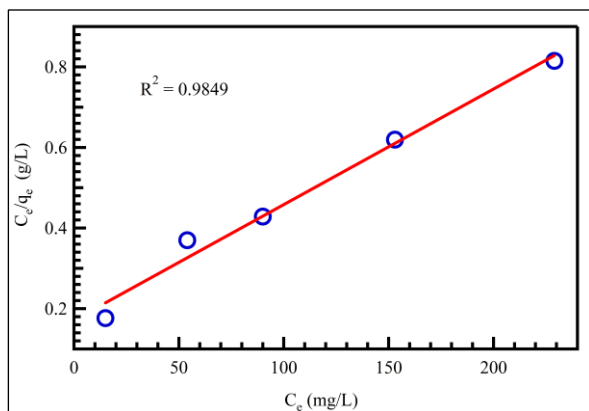


Figure 5. Langmuir adsorption isotherm of H_2S adsorption onto ACES

Table 3. Parameters of Langmuir and Freundlich adsorption isotherm models of H_2S adsorption onto ACES

Langmuir			Freundlich		
Q_{max} (mg/g)	K_L (L/mg)	R^2	K_F (mg/g (L/mg) $^{1/n}$)	$1/n$	R^2
289.3	0.02704	0.97	25.16	0.452	0.984

According to Freundlich isotherm plot ($\log q_e$ vs. $\log C_e$), $1/n$ of 0.452 could be obtained from the slope the straight line gives as shown in Figure 6, showing that the adsorption of H_2S on the ACES is favorable. Accordingly, the Freundlich constants K_F and n are reported in Table 3. R^2 is 0.984, indicating that the fitting error is lower than that of the Langmuir model. Table 4 compares the adsorption capacities of various adsorbents. It is interesting to see that the ACES has the highest adsorption capacity as compared to other adsorbents reported in the literature.

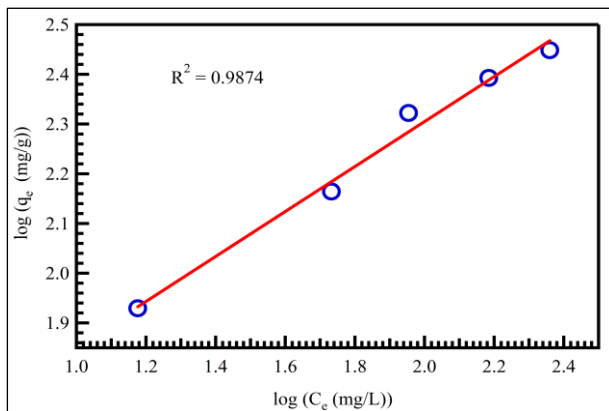


Figure 6. Freundlich adsorption isotherm of H_2S adsorption onto ACES

Table 4. Comparison of maximum monolayer adsorption capacity of dissolved H₂S on various adsorbents

Adsorbent	Adsorbate	Adsorption Capacity (mg/g)	References
Carbon derived from eggshells	H ₂ S	281	This work
IAC under anaerobic conditions	H ₂ S	9.4	[34]
Fine rubber particle media	H ₂ S	0.12	[17]
Crushed oyster shell	H ₂ S	12	[18]
Red mud	H ₂ S	17	[35]
Carbonated steel slag	H ₂ S	7.5	[36]
Activated carbon from sawdust pellets	H ₂ S	6.2	[37]

Adsorption Kinetics

The relation between $\log(q_e - q_t)$ and time showed straight lines as displayed in Figure 7a for the pseudo-first-order kinetic model. R^2 and k_1 values are listed in Table 5. On the other hand, linear relationships were obtained by plotting t/q_t versus t (Figure 7b) for the pseudo-second-order kinetic model. Moreover, the q_e and k_2 were determined from the slope and the intercept of the plot and listed in Table 5.

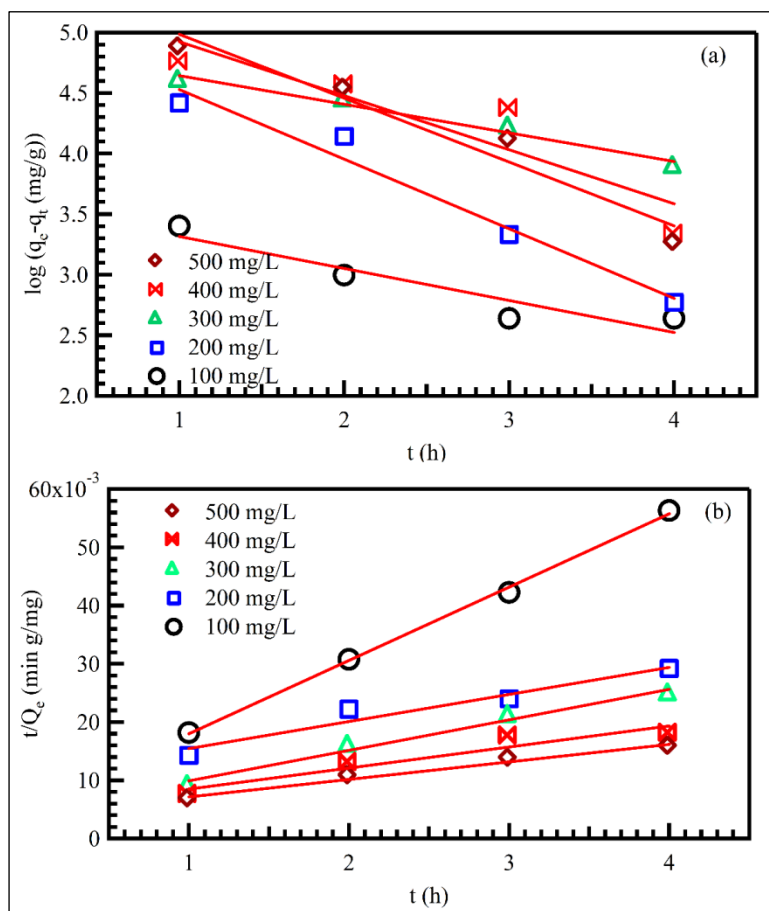


Figure 7. Pseudo-first-order (a) and pseudo-second-order (b) models of H₂S adsorption onto ACES

Table 5. Pseudo-first-order and pseudo-second-order kinetic models' parameters for adsorption of H₂S onto ACES

Kinetic Model	Parameter	Initial H ₂ S Concentration (mg/L)				
		100	200	300	400	500
Pseudo-first-order kinetic model	K ₁ (1/h)	0.264	0.574	0.236	0.445	0.527
	R ²	0.884	0.970	0.820	0.950	0.970
Pseudo-second-order kinetic model	K ₂ (g/mg h)	0.024	0.002	0.005	0.002	0.002
	R ²	0.998	0.943	0.981	0.907	0.980

This procedure is more likely to predict the behavior over the whole range of adsorption. It shows a good agreement between the experimental and the calculated q_e values (Table 5). It is found that, the correlation coefficients for the second-order kinetic model were higher than those for the pseudo-first-order model, indicating the applicability of the second-order kinetic model to describe the adsorption process of H₂S onto the prepared ACES. R² values obtained are shown in Table 5 and they are low compared to those obtained from pseudo-second-order. Table 5 lists the calculated parameters and it is found that the adsorption of H₂S on ACES could be best described by the second-order kinetic model.

Conclusion

The activated carbons have been prepared and analyzed to characterize their physical and chemical properties. The resulting solid samples have been used in the adsorption process of dissolved hydrogen sulfide from aqueous solution. From the current study, the activated carbon derived from the eggshell has the maximum adsorption capacity of 289.3 mg/g which is the highest amongst the other adsorbents reported earlier. The result indicate also that the initial concentration has an important role in the adsorption capacity. The adsorption isotherm fit very well to the well-known Freundlich isotherm model. In addition, the process followed the pseudo-second-order kinetic model. Thus, it can be concluded that eggshell is a very useful green and economic adsorbent due to its good accessibility and absence of any toxic and hazardous elements. Therefore, it is a very suitable candidate for removing H₂S from wastewater.

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